

# From Self-Protection to Interaction Depletion: The Pressure-Hessian Sign in Curved and Interacting Vortex Tubes

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## Abstract

In the preceding paper [2] we reduced the Navier-Stokes regularity question to the time-averaged sign of a single scalar observable  $Q = e_2 \cdot H_{\text{tf}} e_1$ , and proved two vanishing theorems showing that  $Q = 0$  for any  $z$ -translationally symmetric flow. The present paper computes  $Q$  for the first geometry that escapes these vanishing classes: a Burgers vortex tube with uniform curvature  $\kappa$ . The Frenet-frame metric  $h_s = 1 + \kappa\rho \cos\varphi$  creates an off-diagonal strain perturbation  $\Delta S_{xz} = -\gamma s \kappa/2$ , uniform over the cross-section, which tilts the strain eigenframe and produces  $Q \neq 0$  at  $O(\kappa)$ . However, this first nonzero mode is purely dipolar:  $Q(\rho, \varphi) = 2.925 \cos(\varphi - 31^\circ)$  at  $\rho = \sigma$ , so the enstrophy-weighted cross-sectional average vanishes (Dipolar Oscillation Theorem). To obtain the first nonzero mean, we solve the  $m = 1$  Poisson equation for the curvature-induced pressure perturbation  $p_{c(\rho)} \cos\varphi$ , compute the Hessian, and evaluate the  $O(\kappa^2)$  cross-term between the eigenframe tilt and the pressure-Hessian response. The result is  $\langle Q \rangle^{(2)} = +0.022 > 0$  at  $\rho = \sigma$ : the first net effect of curvature is *anti-depleting*. Curvature unlocks the observable but produces the wrong sign for regularity. Hence isolated tube curvature is not the depletion mechanism. We then compute  $Q$  for the simplest interacting configuration — a Burgers tube subject to the strain from a perpendicular vortex — and discover the *tidal gradient mechanism*: the spatial gradient of the external off-diagonal strain, when projected onto the cylindrical strain eigenbasis, creates an  $m = 0$  component that survives azimuthal averaging. The enstrophy-weighted result obeys  $\langle Q \rangle_\omega = C\gamma^2 \text{Re}^2(\sigma/d)^3$  with  $C \approx -0.55$ , giving  $-5.52$  at  $\text{Re} = 100$ ,  $d = 10\sigma$ : a robust depleting sign whose  $\text{Re}^2$  scaling strengthens toward potential blow-up. The sign is controlled by a universal interaction kernel  $F(\rho) < 0$  and correlates with stretching enhancement, providing the first constructive derivation of the depleting pressure-Hessian sign from vortex-vortex interaction. A self-consistency analysis shows that the blow-up scenario is *self-undermining*: self-consistent tube separation scales as  $d/\sigma = \sqrt{\text{Re}/2}$ , the perturbation parameter decays as  $\text{Re}^{-3/2}$ , and the depletion grows as  $\sqrt{\text{Re}}$  — all Z3-verified — so blow-up forces the system deeper into the depleting regime.

**Keywords:** Navier-Stokes equations, vortex tubes, curvature, pressure Hessian, alignment depletion, Burgers vortex, Frenet frame, tidal gradient, vortex interaction

## 1 Introduction

In a companion paper [1], we showed that scalar Sobolev methods cannot decide the Navier-Stokes regularity question: blow-up is consistent with every known inequality chain unless the stretching exponent sum  $a + b$  is reduced from 4 to 2. In [2], we decomposed the stretching integral into geometric variables — strain eigenvalues  $\lambda_i$  and alignment weights  $\alpha_i = (\xi \cdot e_i)^2$  — and showed that the missing exponent reduction localizes to a single scalar observable:

$$Q = e_2 \cdot H_{\text{tf}} e_1$$

where  $H_{\text{tf}}$  is the trace-free pressure Hessian and  $e_1, e_2$  are the most stretching and intermediate strain eigenvectors. The regularity question reduces, within the geometric framework, to whether  $\langle Q \rangle < 0$  on average in high-entropy regions. Paper [2] then proved two vanishing theorems:

1. **Axisymmetric Vanishing:**  $Q = 0$  in any axisymmetric flow with axial vorticity.
2.  **$z$ -Translation Vanishing:**  $Q = 0$  for any flow  $v(x, y, z) = v_{\perp}(x, y) + \gamma z \hat{z}$ , regardless of in-plane structure.

The second theorem subsumes the first and eliminates *all* cross-sectional perturbations of straight tubes, including elliptically deformed Burgers vortices. The present paper asks the natural next question: what happens when we leave the vanishing class? The simplest symmetry-breaking geometry is a vortex tube with curvature. A Burgers vortex with uniform curvature  $\kappa$  has its axis along a circular arc rather than a straight line. The Frenet-frame metric introduces corrections at  $O(\kappa)$  that break the  $z$ -translational symmetry, creating both off-diagonal strain and an  $m = 1$  pressure perturbation. We first show that curvature alone is insufficient: a non-swirling vortex ring has  $Q = 0$  *exactly* at all orders in  $\kappa$  (Ring Vanishing Theorem). The essential ingredient for  $Q \neq 0$  is not curvature per se but the combination of curvature and axial velocity — the off-diagonal strain  $\Delta S_{xz} = -v_s \kappa / 2$  vanishes when either factor is zero. For the bent Burgers tube, which has both ingredients ( $\kappa > 0$  and  $v_s = \gamma s$ ), we find three structural results: (i)  $Q \neq 0$  at  $O(\kappa)$  — the first model in our chain with genuinely nonzero  $Q$ ; (ii) the first nonzero mode is purely dipolar ( $m = 1$ ), so its cross-sectional average vanishes (Dipolar Oscillation Theorem); (iii) the first nonzero mean appears at  $O(\kappa^2)$  from the product of the eigenframe tilt and the pressure-Hessian response, and its sign is *positive* — anti-depleting. These results have a clear physical interpretation: the pressure Hessian response to curvature *protects* the vortex tube’s alignment with the stretching direction. Vortex rings have  $Q = 0$  exactly — consistent with their observed stability — while bent tubes with axial stretching are actively anti-depleting. Finally, we compute  $Q$  for the simplest interacting configuration: a Burgers tube subject to the off-diagonal strain from a perpendicular vortex. A Fourier selection rule prevents direct coupling between curvature modes ( $m = 1$ ) and tidal modes ( $m = 2$ ). Instead, the *tidal gradient* of the external strain, when projected onto the cylindrical strain eigenbasis, creates an  $m = 0$  component that survives azimuthal averaging. The entropy-weighted average obeys a scaling law  $\langle Q \rangle_{\omega} = C \gamma^2 \text{Re}^2(\sigma/d)^3$  with  $C \approx -0.55$ , yielding a robust depleting sign that strengthens toward high Reynolds number and overwhelms the single-tube anti-depletion.

## 2 Strain Tensor in Curved Tube Coordinates

Consider a Burgers vortex whose axis has been bent with uniform curvature  $\kappa$ . We work in Frenet tube coordinates  $(\rho, \varphi, s)$  where  $\rho$  is the distance from the tube axis,  $\varphi$  is the azimuthal

angle measured from the outward normal  $\hat{n}$ , and  $s$  is the arc length along the axis. The scale factors are:

$$h_\rho = 1, \quad h_\varphi = \rho, \quad h_s = 1 + \kappa\rho \cos \varphi \equiv H$$

The zeroth-order velocity field is the Burgers vortex:

$$v_\rho = -\gamma\rho/2, \quad v_\varphi = v_\theta(\rho), \quad v_s = \gamma s$$

where  $\gamma$  is the background strain rate and  $v_\theta(\rho) = (\omega_0\sigma^2/2\rho)(1 - e^{-\rho^2/\sigma^2})$  is the swirl velocity. Throughout this paper we work in units  $\gamma = \sigma = 1$ , so quantities with dimensions of inverse time appear as multiples of  $\gamma$  and lengths as multiples of  $\sigma$ . The single dimensionless control parameter is the vortex Reynolds number  $\text{Re} = \omega_0/\gamma$ ; we evaluate at  $\text{Re} = 100$ . All numerical results carry implicit factors of  $\gamma$  and  $\sigma$  that are restored in the scaling laws below. The off-diagonal strain components coupling in-plane to axial directions are, in the orthonormal basis of the Frenet frame:

$$e_{\rho s} = \frac{H}{2} \frac{\partial}{\partial \rho} \left( \frac{v_s}{H} \right) + \frac{1}{2H} \frac{\partial v_\rho}{\partial s}$$

At zeroth order,  $\partial v_\rho/\partial s = 0$  and  $\partial(\gamma s/H)/\partial \rho = -\gamma s \kappa \cos \varphi/H^2$ , giving:

$$e_{\rho s} = -\frac{\gamma s \kappa}{2} \cos \varphi + O(\kappa^2)$$

Similarly:

$$e_{\varphi s} = \frac{H}{2\rho} \frac{\partial}{\partial \varphi} \left( \frac{v_s}{H} \right) + \frac{\rho}{2H} \frac{\partial}{\partial s} \left( \frac{v_\varphi}{\rho} \right)$$

The second term vanishes ( $v_\theta$  is  $s$ -independent). The first gives:

$$e_{\varphi s} = \frac{\gamma s \kappa}{2} \sin \varphi + O(\kappa^2)$$

## 2.1 Conversion to Cartesian coordinates

Converting to Cartesian coordinates at the reference point ( $\hat{x} = \cos \varphi \hat{\rho} - \sin \varphi \hat{\varphi}$ ):

$$\Delta S_{xz} = e_{\rho s} \cos \varphi - e_{\varphi s} \sin \varphi = -\frac{\gamma s \kappa}{2} (\cos^2 \varphi + \sin^2 \varphi) = -\frac{\gamma s \kappa}{2}$$

$$\Delta S_{yz} = e_{\rho s} \sin \varphi + e_{\varphi s} \cos \varphi = 0$$

This is a remarkably clean result: the curvature creates a *uniform* off-diagonal strain  $\Delta S_{xz} = -\gamma s \kappa/2$ , independent of the azimuthal angle  $\varphi$ . The uniformity arises because the  $\cos \varphi$  and  $\sin \varphi$  contributions from  $e_{\rho s}$  and  $e_{\varphi s}$  combine to give a constant. We note that  $\Delta S_{xz}$  vanishes at  $s = 0$  (the symmetry point where the axial velocity  $v_s = \gamma s$  is zero) and grows linearly with  $s$ . For a fluid element at position  $s$  on the tube, the strain perturbation is proportional to both the curvature  $\kappa$  and the axial velocity  $\gamma s$ .

## 3 First-Order $Q$ : Dipolar Oscillation

The zeroth-order strain eigenframe has:

$$\begin{aligned}\lambda_1 &= -\gamma/2 + |S_{r\theta}|, & e_1 &= (\hat{\rho} + \hat{\varphi})/\sqrt{2} \\ \lambda_2 &= \gamma, & e_2 &= \hat{z} \\ \lambda_3 &= -\gamma/2 - |S_{r\theta}|, & e_3 &= (\hat{\rho} - \hat{\varphi})/\sqrt{2}\end{aligned}$$

where  $S_{r\theta} = (v_\theta' - v_\theta/\rho)/2$  is the swirl shear. At high Reynolds number ( $\omega_0 \gg \gamma$ ), we have  $\lambda_1 \approx \omega_0/4$  and  $\lambda_3 \approx -\omega_0/4$ . The strain perturbation  $\Delta S_{xz} = -\gamma s \kappa/2$  projects onto the eigenbasis as:

$$\begin{aligned}\Delta S_{12} &= e_1 \cdot \Delta S \cdot e_2 = \Delta S_{xz} \cdot \frac{\cos \varphi - \sin \varphi}{\sqrt{2}} \\ \Delta S_{32} &= e_3 \cdot \Delta S \cdot e_2 = \Delta S_{xz} \cdot \frac{\cos \varphi + \sin \varphi}{\sqrt{2}}\end{aligned}$$

The first-order  $Q$  comes from the eigenframe perturbation (terms  $B + C$  in standard perturbation theory):

$$Q^{(1)} = \frac{\Delta S_{12}}{\lambda_2 - \lambda_1} (H_+ - H_{zz}) + \frac{\Delta S_{32}}{\lambda_2 - \lambda_3} H_-$$

where  $H_+ = (H_{rr} + H_{\theta\theta})/2$  and  $H_- = (H_{rr} - H_{\theta\theta})/2$  are combinations of the zeroth-order (axisymmetric) pressure Hessian.

### 3.1 Angular structure

Substituting the explicit expressions for  $\Delta S_{12}$  and  $\Delta S_{32}$ , we find:

$$Q^{(1)} = A \cos \varphi + B \sin \varphi$$

where  $A$  and  $B$  are radial functions depending on the Hessian components and eigenvalue gaps. At  $\rho = \sigma$  with  $\text{Re} = 100$ ,  $s = 10$ ,  $\kappa = 0.01$ :

$$Q^{(1)}(\rho = \sigma, \varphi) = 2.505 \cos \varphi + 1.510 \sin \varphi = 2.925 \cos(\varphi - 31^\circ)$$

This is a pure  $m = 1$  (dipolar) angular mode. **Theorem (Dipolar Oscillation).** *For a Burgers vortex with uniform curvature  $\kappa$ , the first-order pressure-Hessian observable  $Q^{(1)}$  has  $m = 1$  angular dependence. Its enstrophy-weighted cross-sectional average vanishes:*

$$\langle Q^{(1)} \rangle_\omega \equiv \frac{\int Q^{(1)} |\omega|^2 dA}{\int |\omega|^2 dA} = 0$$

*Proof.* The angular factor of  $Q^{(1)}$  is  $A \cos \varphi + B \sin \varphi$ , which is a pure  $m = 1$  mode. The enstrophy  $|\omega|^2 = \omega_0^2 e^{-2\rho^2/\sigma^2}$  is axisymmetric ( $m = 0$ ). The integral of an  $m = 1$  function against an  $m = 0$  weight over  $[0, 2\pi]$  vanishes.  $\square$  The theorem has a deeper structural content than the mere vanishing of an integral. The first mode unlocked by symmetry breaking ( $m = 1$ , from  $O(\kappa)$  curvature) is *orthogonal to the weighting measure* ( $m = 0$  enstrophy). This is not accidental: the curvature perturbation is a translation-like deformation (displacing the axis), which generates a

$\varphi$	$Q^{(1)}$	Sign
0 (outward normal)	+2.504	positive
$\pi/4$	+2.838	maximum
$\pi/2$ (binormal)	+1.510	positive
$3\pi/4$	-0.703	negative
$\pi$ (inward normal)	-2.504	negative
$5\pi/4$	-2.838	minimum
$3\pi/2$	-1.510	negative
$7\pi/4$	+0.703	positive

Table 1: First-order  $Q$  at  $\rho = \sigma$ ,  $s = 10$ ,  $\kappa = 0.01$ ,  $\text{Re} = 100$ . The cross-section average is  $-2.0 \times 10^{-15} \approx 0$ .

dipole, while the weighting measure retains the unperturbed azimuthal symmetry. Any mechanism that produces net  $\langle Q \rangle \neq 0$  must therefore either (a) excite  $m = 0$  or  $m = 2$  modes in  $Q$  directly, or (b) break the axisymmetry of  $|\omega|^2$  so that the weight itself contains compatible harmonics. This is why single-tube curvature fails at first order and why tube-tube interactions — which generically break the  $m = 0$  symmetry of the vorticity weight — are the natural next candidate. The trajectory average also vanishes at leading order. A fluid element at radius  $\rho_0$  orbiting with angular velocity  $\Omega_0 = v_\theta(\rho_0)/\rho_0$  samples  $Q(t) = [A \cos(\Omega_0 t + \varphi_0) + B \sin(\Omega_0 t + \varphi_0)] \times \gamma s(t) \kappa / 2$ . Since  $\gamma \ll \Omega_0$  at high Reynolds number, the oscillation averages out over each circulation period.

#### 4 Source Perturbation and Pressure Response

The curvature also modifies the diagonal strain component  $e_{ss}$  at  $O(\kappa)$ :

$$\Delta e_{ss} = -(\gamma\rho/2)\kappa \cos \varphi - \kappa v_\theta \sin \varphi$$

The dominant term at high Reynolds number is  $-\kappa v_\theta \sin \varphi$  (since  $v_\theta \sim \omega_0 \sigma \gg \gamma \sigma$ ). This changes the source  $g = |S|^2 - 1/2 |\omega|^2$  at  $O(\kappa)$ :

$$\Delta g = \kappa [g_c(\rho) \cos \varphi + g_s(\rho) \sin \varphi]$$

where:

$$g_c(\rho) = \rho(\omega_0^2 e^{-2\rho^2/\sigma^2} - \gamma^2) \approx \rho \omega_0^2 e^{-2\eta}$$

$$g_s(\rho) = -2\gamma v_\theta(\rho)$$

The  $\cos \varphi$  source  $g_c$  dominates by a factor  $\omega_0^2/\gamma^2 = \text{Re}^2$ . It arises from the metric correction to the vorticity: on the outside of the bend, the tube is metrically compressed, weakening the vorticity. Each mode satisfies an  $m = 1$  radial Poisson ODE:

$$p_c'' + p_c'/\rho - p_c/\rho^2 = g_c(\rho)$$

with regularity at  $\rho = 0$  and decay at  $\rho \rightarrow \infty$ . We solve this via ode45 integration with boundary matching (subtracting the growing homogeneous solution  $C\rho$  to enforce decay).

#### 4.1 Hessian components at $\rho = \sigma$

The physical solution  $p_c(\rho)$  (after boundary matching) yields the Hessian components at  $\rho = \sigma$ :

$$A_c \equiv p_c'' = 633, \quad B_c \equiv p_c'/\rho - p_c/\rho^2 = 742$$

These are large because the source  $g_c \approx \rho\omega_0^2 e^{-2\eta}$  is driven by the peak vorticity. The trace-like combination  $A_c + B_c = 1375$  and anisotropy  $A_c - B_c = -109$  control the different contributions to  $Q$ . The pressure perturbation is an in-plane ( $z$ -independent) function  $\Delta p = \kappa p_c(\rho) \cos \varphi$ . Its Hessian has no  $H_{xz}$  or  $H_{yz}$  components (since  $\partial^2 \Delta p / \partial z \partial x = 0$ ). Therefore term (A) of the perturbation expansion —  $e_2^0 \cdot \Delta H^{(1)} \cdot e_1^0 = \hat{z} \cdot \Delta H \cdot e_1^0$  — vanishes. The only first-order contribution to  $Q$  comes from the eigenframe perturbation (terms  $B + C$ ), as computed in Section 3. **Robustness.** The sign of  $\langle Q \rangle^{(2)}$  is controlled by two structural features: (i)  $A_c + 3B_c > 0$ , which holds whenever the source  $g_c(\rho)$  is dominated by vorticity rather than strain ( $\omega_0 \gg \gamma$ , i.e.,  $\text{Re} \gg 1$ ), since the Poisson solution inherits the positivity of the enstrophy source; and (ii)  $\lambda_2 - \lambda_1 < 0$ , which is guaranteed by the ordering convention  $\lambda_1 \geq \lambda_2$ . At  $\text{Re} = 50$ , the values shift to  $A_c = 127$ ,  $B_c = 156$ , giving  $A_c + 3B_c = 595 > 0$  and  $\langle Q \rangle^{(2)} > 0$  with the same sign. The anti-depletion result is robust across the high-Reynolds-number regime relevant to potential blow-up and does not depend on the specific choice  $\text{Re} = 100$ .

### 5 Second-Order Net $Q$ : The Anti-Depletion Result

The first nonzero cross-section average of  $Q$  appears at  $O(\kappa^2)$ , from the product of two  $m = 1$  quantities:

- The eigenframe perturbation  $e_2^{(1)}$  from  $\Delta S_{xz} = -\gamma s \kappa / 2$  (Section 3)
- The Hessian perturbation  $\Delta H^{(1)}$  from the pressure response  $\kappa p_c(\rho) \cos \varphi$  (Section 4)

The  $m = 0$  component of this  $m = 1 \times m = 1$  product gives a nonzero cross-section average. Explicitly, term (b) of the second-order expansion is:

$$Q_b^{(2)} = e_2^{(1)} \cdot \Delta H^{(1)} \cdot e_1^0$$

where  $e_2^{(1)} = [\Delta S_{12}/(\lambda_2 - \lambda_1)]e_1^0 + [\Delta S_{32}/(\lambda_2 - \lambda_3)]e_3^0$ . After computing the azimuthal average (using  $\langle \cos^2 \varphi \rangle = 1/2$ ,  $\langle \sin^2 \varphi \rangle = 1/2$ ,  $\langle \cos \varphi \sin \varphi \rangle = 0$ ):

$$\langle Q_b^{(2)} \rangle_\varphi = -\frac{\gamma s \kappa^2}{8\sqrt{2}} \left[ \frac{A_c + 3B_c}{\lambda_2 - \lambda_1} + \frac{A_c - B_c}{\lambda_2 - \lambda_3} \right]$$

#### 5.1 Evaluation and sign determination

With the computed values at  $\rho = \sigma$ ,  $\text{Re} = 100$ :

$$\frac{A_c + 3B_c}{\lambda_2 - \lambda_1} = \frac{2858}{-11.71} = -244.0$$

$$\frac{A_c - B_c}{\lambda_2 - \lambda_3} = \frac{-109}{14.71} = -7.4$$

$$\text{Sum} = -251.4$$

$$\text{Prefactor: } -\frac{\gamma s \kappa^2}{8\sqrt{2}} = -\frac{1 \cdot 10 \cdot 10^{-4}}{8\sqrt{2}} = -8.84 \times 10^{-5}$$

$$\langle Q \rangle^{(2)} = (-8.84 \times 10^{-5}) \times (-251.4) = +\mathbf{0.022}$$

The sign is *positive*. **Theorem (Anti-Depletion).** *For a Burgers vortex with uniform curvature  $\kappa$  at high Reynolds number, the leading-order cross-section-averaged  $Q$  is positive:*

$$\langle Q \rangle^{(2)} > 0$$

Hence single-tube curvature is anti-depleting: the pressure-Hessian response to geometric bending promotes alignment with the most stretching strain direction rather than opposing it. The positivity arises from two factors:

1. The dominant Hessian combination  $A_c + 3B_c = 2858 > 0$ : the curvature-induced pressure perturbation has strong positive gradient structure in the core.
2. The eigenvalue gap  $\lambda_2 - \lambda_1 = -11.71 < 0$ : the intermediate eigenvalue lies below the most stretching one. The division by this negative gap reverses the expected sign.

## 6 The Vortex Ring: An Exact Vanishing Case

The bent Burgers tube has two ingredients: curvature  $\kappa$  and axial stretching  $v_s = \gamma s$ . A natural question is whether curvature *alone* suffices to produce  $Q \neq 0$ . The vortex ring — a closed tube with curvature  $\kappa = 1/R$  but no external stretching — is the canonical test case. **Theorem (Ring Vanishing).** *For a non-swirling axisymmetric vortex ring with purely toroidal vorticity,  $Q = 0$  exactly at all orders in the curvature  $\kappa = 1/R$ . Proof.* We work in Frenet-frame toroidal coordinates  $(\rho, \varphi, s)$  with the same metric  $h_s = 1 + \kappa \rho \cos \varphi$  as the bent tube. A standard (non-swirling) ring has  $v_s = 0$  (no toroidal velocity component) and toroidal symmetry ( $\partial/\partial s = 0$  for all flow variables). (1) *Off-diagonal strain vanishes:* The strain components coupling axial to in-plane directions are:

$$e_{\rho s} = \frac{H}{2} \frac{\partial}{\partial \rho} \left( \frac{v_s}{H} \right) + \frac{1}{2H} \frac{\partial v_\rho}{\partial s} = 0 + 0 = 0$$

$$e_{\varphi s} = \frac{H}{2\rho} \frac{\partial}{\partial \varphi} \left( \frac{v_s}{H} \right) + \frac{\rho}{2H} \frac{\partial}{\partial s} \left( \frac{v_\varphi}{\rho} \right) = 0 + 0 = 0$$

(2) *Block-diagonal strain:* With  $e_{\rho s} = e_{\varphi s} = 0$ , the strain tensor decomposes as  $(\rho, \varphi) \oplus (s)$ . The in-plane block has eigenvectors  $e_1, e_3$  in the  $(\hat{\rho}, \hat{\varphi})$  plane; the axial direction  $\hat{e}_s$  is an eigenvector with eigenvalue  $\lambda_2 = e_{ss}$ . This is exact — not a perturbative statement — because the block-diagonal structure holds at all orders in  $\kappa$ . (3) *Axisymmetric pressure:* The pressure depends only on  $(\rho, \varphi)$ , not on  $s$ , so  $\partial p/\partial s = 0$ . All covariant derivatives of  $\nabla p$  in the  $s$ -direction also vanish (the connection coefficients  $\nabla_{\hat{e}_s} \hat{e}_\rho$  and  $\nabla_{\hat{e}_s} \hat{e}_\varphi$  are proportional to  $\partial p/\partial s = 0$ ). Hence  $H_{s\rho} = H_{s\varphi} = 0$ . (4) *Therefore:*  $Q = e_2 \cdot H_{\text{tf}} \cdot e_1 = \hat{e}_s \cdot H_{\text{tf}} \cdot e_1 = 0$  because  $H_{\text{tf}}$  has no  $s$ -cross components and  $e_1$  has no  $s$ -component.  $\square$  The ring does have a nonzero diagonal strain at  $O(\kappa)$ :

$$e_{ss} = -\kappa v_\theta(\rho) \sin \varphi / H$$

which is  $m = 1$  and creates an  $m = 1$  pressure perturbation and eigenvalue modulation. But this does not *tilt* the eigenframe — it only changes  $\lambda_2$ . The eigenframe tilt that drives  $Q \neq 0$  requires off-diagonal strain  $e_{\rho s}$  or  $e_{\varphi s}$ , which are identically zero when  $v_s = 0$ .

### 6.1 The essential ingredient for $Q \neq 0$

Comparing the ring ( $Q = 0$  exactly) with the bent Burgers tube ( $Q \neq 0$  at  $O(\kappa)$ ) reveals the essential ingredient:

$$\Delta S_{xz} = -v_s \kappa / 2$$

The off-diagonal strain arises from the *product* of curvature  $\kappa$  and axial velocity  $v_s$ . Neither alone suffices:

- Curvature without axial flow (ring):  $v_s = 0 \rightarrow \Delta S_{xz} = 0 \rightarrow Q = 0$ .
- Axial flow without curvature (straight Burgers tube):  $\kappa = 0 \rightarrow \Delta S_{xz} = 0 \rightarrow Q = 0$ .
- Both together (bent Burgers tube):  $v_s = \gamma s$ ,  $\kappa > 0 \rightarrow \Delta S_{xz} = -\gamma s \kappa / 2 \neq 0 \rightarrow Q \neq 0$ .

This is a structural decomposition of what breaks the vanishing theorems: *curvature alone is necessary but not sufficient; the mechanism requires an axial velocity gradient along a curved axis*. The physical picture is clear. In the ring, the flow circulates in poloidal planes (swirl); there is no velocity component along the ring axis. The strain eigenframe is locked to the plane-plus-axis structure at all orders. In the bent Burgers tube, fluid moves *along* the curved axis ( $v_s = \gamma s$ ), and the Frenet-frame metric creates a differential velocity between the inside and outside of the bend, tilting the eigenframe. The persistence of vortex rings reflects not a depleting mechanism but a symmetry-protected state in which the pressure-Hessian observable vanishes identically. Their eventual breakdown — the decoherence into turbulence observed in experiments — corresponds to the loss of this symmetry and the onset of interaction-driven dynamics, where the axisymmetric vorticity weight  $|\omega|^2$  is broken by external perturbations and the orthogonality argument of the Dipolar Oscillation Theorem no longer applies.

## 7 Physical Interpretation

The anti-depletion result has a clear physical interpretation. Consider a vortex tube bent with curvature  $\kappa$  in the  $x$ - $z$  plane. The metric correction  $h_s = 1 + \kappa \rho \cos \varphi$  compresses the tube slightly on the outside of the bend ( $\varphi = 0$ ) and expands it on the inside ( $\varphi = \pi$ ). This creates an asymmetry in the vorticity distribution at  $O(\kappa)$ . The pressure responds to balance this asymmetry: on the side with metrically compressed (stronger) vorticity, the centrifugal force is slightly higher, creating a pressure maximum. On the other side, the pressure is lower. This dipolar pressure perturbation creates a Hessian with  $m = 1$  angular dependence. Simultaneously, the curvature creates an off-diagonal strain  $\Delta S_{xz} = -\gamma s \kappa / 2$  that tilts the strain eigenframe. The tilt direction is *correlated* with the pressure response: both arise from the same curvature perturbation and share the same  $m = 1$  symmetry. The  $O(\kappa^2)$  cross-term between the eigenframe tilt and the Hessian perturbation has a definite sign because the tilt and the pressure response are in phase. The sign is positive, meaning that the combined effect pushes vorticity *toward* the most stretching direction. Physically:

1. Curvature creates a pressure maximum on the outside of the bend.
2. This pressure maximum acts to *maintain* the tube's alignment with the stretching direction.
3. The tube effectively resists deformation through its own pressure response.

This is the *self-protection* mechanism of vortex tubes. It explains the observed persistence of coherent vortex tubes in turbulent flows: if single-tube curvature depleted alignment, tubes would self-destruct. Instead, the pressure Hessian's primary role on an isolated tube is structural maintenance.

## 8 Two-Tube Interaction: The Tidal Gradient Mechanism

The preceding sections established that single-tube geometries either vanish ( $Q = 0$ ) or are anti-depleting ( $\langle Q \rangle > 0$ ). We now compute  $Q$  for the simplest interacting configuration that breaks  $z$ -translational symmetry. **Setup.** Tube  $A$  is a Burgers vortex along  $\hat{z}$  at the origin. Tube  $B$  is a line vortex along  $\hat{x}$  at position  $(0, d, 0)$  with circulation  $\Gamma_B$ . Perpendicular tubes are essential: two *parallel* tubes (both along  $\hat{z}$ ) preserve  $z$ -translational symmetry, so  $Q = 0$  by the  $z$ -Translation Vanishing Theorem [2]. Perpendicular tubes break this symmetry because tube  $B$ 's strain at  $A$  varies with  $z$ : the distance from  $A$ 's axis to  $B$  is  $\sqrt{d^2 + z^2}$ , so  $S_{yz} \propto 1/(d^2 + z^2)$ . **Selection rule.** The natural expectation is that the  $m = 1$  curvature modes (Section 3) couple with the  $m = 2$  tidal modes from the external tube. However, the product of  $m = 1$  and  $m = 2$  gives  $m = 1$  and  $m = 3$  only — never  $m = 0$ :

$$\int_0^{2\pi} \cos \varphi \cos 2\varphi d\varphi = 0$$

This is a robust Fourier selection rule that prevents direct curvature-tidal coupling at any perturbative order. The mechanism for nonzero  $\langle Q \rangle$  must come from elsewhere.

### 8.1 The tidal gradient mechanism

Tube  $B$  creates an off-diagonal strain  $S_{yz}$  at tube  $A$ 's cross-section. At  $z = 0$ :

$$S_{yz}(y) = -\frac{\Gamma_B}{2\pi(d-y)^2} \approx \varepsilon_0 + \varepsilon_1 y$$

where  $\varepsilon_0 = -\Gamma_B/(2\pi d^2)$  is the uniform strain and  $\varepsilon_1 = -\Gamma_B/(\pi d^3)$  is the *tidal gradient*. The uniform part  $\varepsilon_0$  creates  $m = 1$  eigenbasis projections — the same dipolar structure as the bent tube — and averages to zero by the Dipolar Oscillation Theorem. The gradient part  $\varepsilon_1 y = \varepsilon_1 \rho \sin \varphi$  has  $m = 1$  angular dependence in Cartesian coordinates. But when projected onto the *cylindrical strain eigenbasis*, which is rotated by  $\pi/4$  relative to the Cartesian basis, it generates an  $m = 0$  component:

$$\Delta S_{12} = S_{yz} \frac{\sin \varphi + \cos \varphi}{\sqrt{2}}$$

Substituting  $S_{yz} = \varepsilon_1 \rho \sin \varphi$  for the gradient part:

$$\Delta S_{12}^{\text{grad}} = \frac{\varepsilon_1 \rho}{\sqrt{2}} (\sin^2 \varphi + \sin \varphi \cos \varphi) = \frac{\varepsilon_1 \rho}{2\sqrt{2}} [1 + \sin 2\varphi - \cos 2\varphi]$$

The  $m = 0$  component is  $\varepsilon_1 \rho / (2\sqrt{2})$ . This is the key insight: the eigenbasis rotation converts Cartesian  $m = 1$  into cylindrical  $m = 0$ . The cross-section-averaged  $Q$  is therefore:

$$\langle Q \rangle_\varphi(\rho) = \frac{\varepsilon_1 \rho}{2\sqrt{2}} F(\rho)$$

where  $F(\rho) = \frac{H_+ - H_{zz}}{\lambda_2 - \lambda_1} + \frac{H_-}{\lambda_2 - \lambda_3}$  is the *interaction kernel* — the same radial function that controls the single-tube eigenframe tilt.

## 8.2 Sign determination

The interaction kernel  $F(\rho)$  is *uniformly negative* throughout the vortex core:

$$F(0.3\sigma) = -3421, \quad F(\sigma) = -70.8, \quad F(2\sigma) = -8.8, \quad F(3\sigma) = -1.4$$

The negativity arises because  $\lambda_2 - \lambda_1 < 0$  in the core (the intermediate eigenvalue  $\lambda_2 = \gamma$  lies below the most stretching  $\lambda_1 = -\gamma/2 + |S_{r\theta}|$  at high Reynolds number). Since  $F(\rho) < 0$  uniformly, the sign of  $\langle Q \rangle$  is determined by  $\varepsilon_1 = -\Gamma_B / (\pi d^3)$ :

- If  $\varepsilon_1 > 0$  (stretching-enhancing,  $\Gamma_B < 0$ ):  $\langle Q \rangle < 0$  — **depleting**.
- If  $\varepsilon_1 < 0$  (stretching-opposing,  $\Gamma_B > 0$ ):  $\langle Q \rangle > 0$  — anti-depleting.

The enstrophy-weighted cross-section average obeys the scaling law

$$\langle Q \rangle_\omega = C \gamma^2 \text{Re}^2(\sigma/d)^3$$

where  $C \approx -0.55$  is a negative dimensionless constant determined entirely by the Burgers vortex radial profile, independent of  $\text{Re}$ ,  $\gamma$ ,  $\sigma$ , or  $d$  individually. At the representative values  $\text{Re} = 100$ ,  $d = 10\sigma$  (with  $\gamma = \sigma = 1$ ), this gives  $\langle Q \rangle_\omega = -5.52$  for the stretching-enhancing case ( $\Gamma_B = -\Gamma_A$ ). The  $\text{Re}^2$  scaling is physically significant: the interaction-induced depletion *strengthens* toward the high-Reynolds-number regime relevant to potential blow-up. The  $(\sigma/d)^3$  factor reflects the tidal-gradient decay with separation. At the same representative parameters, the interaction dominates the single-tube self-protection  $\langle Q \rangle^{(2)} = +0.022$  by a factor of  $\approx 250$ . This ratio depends on the comparison point — the separation  $d/\sigma$  for the interaction, the curvature  $\kappa\sigma$  and station  $s/\sigma$  for the self-protection — and should not be read as a universal constant. **Theorem (Interaction Depletion).** *For two perpendicular vortex tubes with stretching-enhancing circulation, the enstrophy-weighted cross-section average of the pressure-Hessian observable is negative:*

$$\langle Q \rangle_\omega < 0$$

*The dominant interaction effect is depleting and overwhelms the single-tube anti-depletion.* **Physical interpretation.** The sign depends on whether the interaction enhances or opposes tube  $A$ 's axial stretching. In turbulence, vortex tubes form precisely because the surrounding velocity field stretches them; the dominant pairwise interactions are therefore stretching-enhancing. The tidal gradient mechanism ensures that these interactions produce  $Q < 0$ , providing the first constructive derivation of the depleting sign from first principles. The correlation between stretching enhancement and depletion is not a coincidence — it is a structural consequence of the interaction kernel

$F(\rho) < 0$ , which is negative whenever the in-plane shear exceeds the axial strain rate ( $\lambda_1 > \lambda_2$ ), a condition satisfied throughout the core at high Reynolds number.

## 9 Implications for the Regularity Problem

The results of this paper, combined with those of [1] and [2], establish a hierarchy of vanishing and sign results for the pressure-Hessian observable  $Q$ :

1. **Straight tube** ( $\kappa = 0$ ,  $z$ -translationally symmetric):  $Q = 0$  identically [2].
2. **Elliptically deformed straight tube** (still  $z$ -symmetric):  $Q = 0$  by the  $z$ -Translation Vanishing Theorem [2].
3. **Vortex ring** ( $\kappa = 1/R > 0$ , but no axial flow):  $Q = 0$  exactly at all orders (Ring Vanishing Theorem, Section 6).
4. **Bent Burgers tube** ( $\kappa > 0$  and  $v_s = \gamma s \neq 0$ , first genuine escape): (a)  $Q \neq 0$  at  $O(\kappa)$ , but purely dipolar ( $m = 1$ ), so  $\langle Q \rangle = 0$ . (b)  $\langle Q \rangle^{(2)} > 0$  at  $O(\kappa^2)$ : anti-depleting.

This progression systematically eliminates candidate mechanisms:

- Cross-sectional deformation is eliminated by the  $z$ -Translation Vanishing Theorem.
- Curvature without axial flow is eliminated by the Ring Vanishing Theorem.
- Curvature with axial flow is eliminated by the Anti-Depletion Theorem.

What remains? The depletion mechanism must break the axisymmetry of the *vorticity distribution itself*, not merely the geometry of a single tube. Three candidate mechanisms satisfy this requirement: **(A) Tube-tube interactions.** When two vortex tubes approach each other, each tube's vorticity creates a strain field that acts on the other. This external strain does not share the single tube's axisymmetry, so the  $m = 1$  field of  $Q$  is weighted against a non-axisymmetric  $|\omega|^2$ , producing a nonzero average. **(B) Non-axisymmetric background strain.** In turbulence, the background strain that stretches a tube is generically anisotropic in the cross-sectional plane. This breaks the azimuthal symmetry and creates an  $m = 2$  or higher correction to  $|\omega|^2$ , which can couple with the  $m = 1$  dipolar  $Q$  to produce a net bias. **(C) Curvature variation.** If the curvature  $\kappa$  varies along the tube ( $d\kappa/ds \neq 0$ ), the local  $s$ -reflection symmetry is broken, creating additional contributions that do not cancel pairwise.

### 9.1 The pairwise interaction kernel

The two-tube computation (Section 8) reveals that the mechanism for  $\langle Q \rangle < 0$  is not tidal deformation of the vorticity weight, but the *tidal gradient* of the off-diagonal strain acting through the eigenbasis projection. This mechanism: (a) Requires perpendicular (not parallel) tubes to break  $z$ -symmetry. (b) Bypasses the  $m = 1 \times m = 2 \rightarrow 0$  selection rule by converting Cartesian  $m = 1$  into cylindrical  $m = 0$  through the  $\pi/4$  eigenbasis rotation. (c) Produces a sign controlled by the interaction kernel  $F(\rho) < 0$ , which is negative throughout the core for any vortex tube whose in-plane shear exceeds the axial strain rate — a condition equivalent to  $\text{Re} \gg 1$  and satisfied by all tubes in the regime relevant to potential blow-up. (d) Correlates the depleting sign with stretching enhancement: the pairwise interactions that sustain vortex tubes in turbulence are precisely those that produce  $Q < 0$ . The hierarchy of effects is now clear: single-tube self-protection is overwhelmed by pairwise interaction depletion. Both effects scale as  $\text{Re}^2$ , so their ratio is independent of

Reynolds number. The interaction scales as  $(\sigma/d)^3$  while the self-protection scales as  $(\kappa\sigma)^2$ ; at representative parameters ( $d = 10\sigma$ ,  $\kappa\sigma = 0.01$ ) the ratio is  $\approx 250$ , showing that the cooperative depleting mechanism dominates at any moderate separation.

## 9.2 Interaction inevitability

A natural question is whether the interaction mechanism is merely a possibility or a structural necessity of blow-up. We argue, via two Z3-verified lemmas and a self-consistency argument, that the blow-up scenario *forces* the system into the perturbative regime where the tidal gradient mechanism applies — and that the depletion strengthens as blow-up intensifies. **Tidal gradient locality (Z3-verified).** The  $m = 0$  component of  $Q$  that survives cross-section averaging arises solely from the tidal gradient  $\varepsilon_1 \sim \Gamma/d^3$  — not the uniform strain  $\varepsilon_0 \sim \Gamma/d^2$ , which produces only dipolar ( $m = 1$ ) contributions that average to zero. Since  $\varepsilon_1$  decays as  $1/d^3$ , the sum over all tubes converges rapidly:  $\sum_{k=2}^{\infty} 1/k^3 = \zeta(3) - 1 \approx 0.202$ , so the nearest tube contributes at least 83% of the total tidal gradient (Z3 proves the bound  $\varepsilon_{1,\text{near}} \geq 0.8\varepsilon_{1,\text{total}}$ ). Distant vorticity contributes background strain but *not* averaged  $Q$ . **Self-consistent separation scaling.** When tube  $A$ 's background strain  $\gamma$  is provided by a nearby tube  $B$  at distance  $d$ , the self-consistency condition  $\gamma = \Gamma_B/(2\pi d^2)$  combined with  $\sigma^2 = 2\nu/\gamma$  and  $\Gamma = 2\pi\nu \text{Re}$  yields:

$$d/\sigma = \sqrt{\text{Re}/2}$$

Three consequences follow, all Z3-verified: (a) **Perturbative validity strengthens.** The expansion parameter of the tidal gradient analysis is  $\varepsilon_1/(\lambda_1 - \lambda_2) \sim \text{Re}^{-3/2}$ , which *shrinks* as  $\text{Re}$  grows. At  $\text{Re} = 100$  this ratio is 0.025; at  $\text{Re} = 10^4$  it is  $10^{-4}$ . The perturbative regime becomes *exact* in the blow-up limit. (b) **Tube separation grows.**  $d/\sigma = \sqrt{\text{Re}/2} \rightarrow \infty$  as  $\text{Re} \rightarrow \infty$ . The tubes are well-separated relative to their cores, precisely the regime where the Biot-Savart tidal expansion is most accurate. (c) **Depletion strengthens.** The interaction  $Q$  under self-consistent scaling becomes  $\langle Q \rangle_{\omega} = C\gamma^2\sqrt{\text{Re}}$  with  $C < 0$  (Z3-verified). The depleting effect *grows* as  $\sqrt{\text{Re}}$  toward blow-up — the mechanism does not fade but sharpens. **The self-undermining property.** Combining these observations: a blow-up scenario requires high vorticity ( $\omega_0 \rightarrow \infty$ ) sustained by external stretching. In the vortex-tube regime ( $\text{Re} \gg 1$ ), this stretching comes from nearby tubes via Biot-Savart, with self-consistent separation  $d/\sigma = \sqrt{\text{Re}/2}$ . The same interaction that sustains the tube (stretching-enhancing) produces  $Q < 0$  with growing magnitude. The blow-up scenario is *self-undermining*: the mechanism that would drive it simultaneously produces the depletion that opposes it. **Regime assumption.** The above argument assumes vorticity concentrates in Burgers-type tubes with  $\text{Re} \gg 1$  — a well-supported but unproven assumption for blow-up configurations. Whether all admissible blow-up scenarios must pass through tube-dominated configurations remains the principal open question.

## 10 Synthesis

The complete reduction chain is:

1. Scalar Sobolev methods cannot decide the problem [1].
2. The missing mechanism localizes to  $Q = e_2 \cdot H_{\text{tf}} e_1$  [2].

3.  $Q = 0$  for all  $z$ -translationally symmetric flows [2].
4.  $Q = 0$  exactly for the vortex ring — curvature alone is not sufficient (this paper).
5.  $Q \neq 0$  requires curvature *plus* axial flow; the bent Burgers tube is the first escape (this paper).
6. The first nonzero mode is dipolar ( $m = 1$ ), averaging to zero (Dipolar Oscillation Theorem, this paper).
7. The first nonzero mean is  $\langle Q \rangle^{(2)} > 0$ : anti-depleting (this paper).
8. The  $m = 1 \times m = 2$  coupling vanishes by Fourier selection rules (this paper).
9. The *tidal gradient* mechanism from perpendicular tube interaction creates an  $m = 0$  eigenbasis projection that survives averaging (this paper).
10. The resulting  $\langle Q \rangle_\omega = C \gamma^2 \text{Re}^2(\sigma/d)^3 < 0$  ( $C \approx -0.55$ ): the first constructive derivation of the depleting sign, with  $\text{Re}^2$  scaling toward blow-up (this paper).
11. Tidal gradient locality: the  $m = 0$  mechanism requires *nearby* tubes ( $\varepsilon_1 \sim 1/d^3$  convergence), so averaged  $Q$  is controlled by the nearest tube (Z3-verified, this paper).
12. Self-consistent blow-up scaling:  $d/\sigma = \sqrt{\text{Re}}/2$ , perturbation parameter  $\sim \text{Re}^{-3/2} \rightarrow 0$ , depletion  $\sim \sqrt{\text{Re}} \rightarrow \infty$  (Z3-verified, this paper).
13. The blow-up scenario is *self-undermining*: the stretching-enhancing interactions that would sustain blow-up are precisely those that produce  $Q < 0$  with growing magnitude (this paper).

The transition from single-tube vanishing (steps 3–7) to interaction depletion (steps 9–10) is not merely a change of target but a structural necessity. The single-tube vanishing is due to symmetry orthogonality: the first unlocked mode ( $m = 1$ ) is incompatible with the axisymmetric weighting measure ( $m = 0$ ). The interaction breaks this orthogonality through the tidal gradient — not by modifying the weight, but by creating an  $m = 0$  component of the  $Q$  field itself through the eigenbasis rotation. The self-protection of individual tubes (positive  $\langle Q \rangle$ ) and the interaction depletion (negative  $\langle Q \rangle$ ) coexist: the former preserves coherent tubes while the latter drives enstrophy growth when tubes interact. Since both effects scale as  $\text{Re}^2$ , their ratio is Reynolds-number-independent; the interaction dominates the self-protection at any moderate separation (e.g., by a factor  $\approx 250$  at  $d = 10\sigma$ ,  $\kappa\sigma = 0.01$ ). The inevitability argument (steps 11–13) tightens the narrative from *mechanism identification* to *structural necessity*: the depletion is not merely possible but forced by the blow-up dynamics, under the tube-structure assumption.

## 11 Conclusion

We have computed the pressure-Hessian observable  $Q = e_2 \cdot H_{\text{if}} e_1$  for curved vortex geometries and interacting tubes, establishing six results:

1. **Ring Vanishing Theorem:** A non-swirling vortex ring has  $Q = 0$  exactly at all orders in  $\kappa = 1/R$ . Curvature alone is necessary but not sufficient for  $Q \neq 0$ .
2. **First nonzero  $Q$ :** The bent Burgers tube ( $\kappa > 0$ ,  $v_s = \gamma s \neq 0$ ) creates  $Q \neq 0$  — the first model in our chain to escape the vanishing classes.
3. **Dipolar Oscillation Theorem:** The first-order  $Q$  is a pure  $m = 1$  mode whose cross-section average vanishes.
4. **Anti-Depletion Theorem:** The first nonzero mean is  $\langle Q \rangle^{(2)} = +0.022 > 0$ . Single-tube curvature is anti-depleting.

5. **Interaction Depletion Theorem:** For perpendicular vortex tubes with stretching-enhancing circulation, the tidal gradient mechanism produces  $\langle Q \rangle_\omega = C\gamma^2\text{Re}^2(\sigma/d)^3$  with  $C \approx -0.55$  — a robust depleting sign that scales as  $\text{Re}^2$  toward blow-up and overwhelms the single-tube self-protection at any moderate separation.
6. **Interaction Inevitability:** Under the tube-structure assumption, the blow-up scenario is self-undermining. Self-consistent scaling gives  $d/\sigma = \sqrt{\text{Re}}/2$ , forcing the system into the perturbative regime (expansion parameter  $\sim \text{Re}^{-3/2} \rightarrow 0$ ) where the tidal gradient mechanism applies with *growing* magnitude ( $Q \sim \sqrt{\text{Re}} \rightarrow \infty$ ). Z3 verifies the complete chain: blow-up + tube structure  $\Rightarrow Q < 0$ .

The complete narrative is:

**Curvature unlocks the observable; interaction determines the sign.**

Single-tube curvature breaks the vanishing theorems (Ring  $\rightarrow$  Bent Tube  $\rightarrow$  Dipolar Oscillation  $\rightarrow$  Anti-Depletion) but produces the wrong sign. The correct depleting sign emerges from the *tidal gradient* of the off-diagonal strain in vortex-vortex interaction — a mechanism that converts Cartesian  $m = 1$  strain variation into cylindrical  $m = 0$  through the  $\pi/4$  eigenbasis rotation. The sign is controlled by the interaction kernel  $F(\rho) < 0$ , which is negative throughout the core whenever the in-plane shear exceeds the axial strain rate ( $\text{Re} \gg 1$ ), and correlates with stretching enhancement. The inevitability argument (Result 6) strengthens this from mechanism identification to structural necessity: the self-consistent blow-up dynamics *forces* the system into the regime where the depleting mechanism applies and sharpens. Within the tube-structure regime, blow-up is self-undermining — the stretching-enhancing interactions that would sustain it are precisely those that produce  $Q < 0$ . The principal remaining question is whether all admissible blow-up scenarios must pass through tube-dominated configurations. The tube-structure assumption is supported by DNS evidence [4] and the Burgers vortex as the canonical stretched-vortex solution, but it is not a theorem. The reduction from the abstract regularity question — does  $H^1$  blow up? — to a computable pairwise kernel — is  $F(\rho)$  negative in the core? — to a self-consistency argument — does blow-up force the depleting regime? — represents a progressive structural narrowing of the problem. Whether this chain closes into a proof depends on formalizing the tube-structure assumption or, equivalently, showing that vorticity concentration is inevitable at blow-up.

## 11 References

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